HALT/HASS Vibration Demystified

Presented by:

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Fostering Revolutionary Thinking

ESTECH™ 2015

IEST®

Fatigue Damage Spectrum

for

HALT & HASS Process
Repetitive Shock Machines
End--Use Environments
Service Life Modeling & Reliability

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BIO

- *President-Smithson & Associates since 1983*
  - *BSME-University of Michigan*
  - *MBA-Arizona State University*

- *Formerly represented*
  - *Screening Systems*
  - *Hobbs Engineering*
  - *Allegan/Hanse Environmental*
  - *QualMark Corporation*

- *Publications*
  - *Effectiveness & Economics-Yardsticks for ESS Decisions—IES Proceedings 1990*
  - *Shock Response Spectrum Analysis for ESS and Strife-HALT--IES Proceedings 1991*
  - *A Viewpoint on Fatigue Metrics-- Benefits for HALT, HASS and More 10th Annual Workshop on Accelerated Stress Testing & Reliability, Chicago, October 2004 & Test Engineering & Management, August-September 2004*
  - -- Correlating HALT & HASS, RS/HALT Vibration and End-Use Environments---Sound & Vibration. March 2015

- *Representing*
  - *Vibration Research*
  - *ETS Solutions*
  - *Vibration & Shock Technologies*
  - *Instrumented Sensor Technologies*

References

- *Svensson, T. and Torstensson, H.O., "Utilization of Fatigue Damage Response Spectrum in the Evaluation of Transport Stresses", to be presented at the IES 1993 ATM, 2-7 May in Las Vegas.*
- *Piersol, A.G., Henderson, G.R., "Fatigue Damage Related Descriptor for Random Vibration Test Equipments," Sound and Vibration Magazine, Vol. 29, No. 10, pp. 20-24,*
- *Van Baren, John and Phillip, "KurtosionTM—Getting the Kurtosis into the Resonances", was presented at SAVIAC 2007.*
- *Gaberson, Howard A., "Pseudo-Velocity Shock Spectrum Rules for Analysis of Mechanical Shock", presented IMAC 2007.*
- *Smithson, Stephen A., "A Viewpoint on Fatigue Metrics-- Benefits for HALT, HASS and More" 10th Annual Workshop on Accelerated Stress Testing & Reliability, Chicago October 2004*
- *Achatz, Thomas M., and Van Baren, John G. , "Using Fatigue Damage Spectrum for Accelerated Testing with Correlation to End-use Environment", 2014 Accelerated Stress Testing & Reliability Workshop, St. Paul 10-12 October 2014*

Trip Down Memory Lane

IEEE Components, Packaging, and Manufacturing Technology Society

IEEE

ASTR 2004

A Viewpoint on Fatigue Metrics--Benefits for HALT, HASS and More

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Abstract

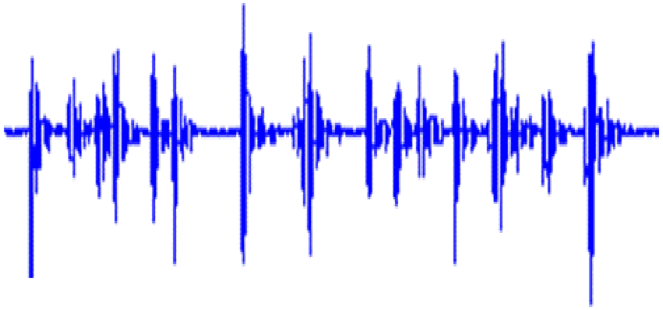
- ***Overcoming decades of shortcomings, applying a Fatigue Damage Spectrum (FDS) to Repetitive Shock (RS) machines used in HALT (Highly Accelerated Life Tests) and HASS (Highly Accelerated Stress Screening) provides a tool for improved use and analysis. FDS can be used to benchmark RS excitations and product responses to correlate them with End-Use-Environments (EUE) and ED shakers, thus quantifying severities of different excitations for Analysis.***

Objective

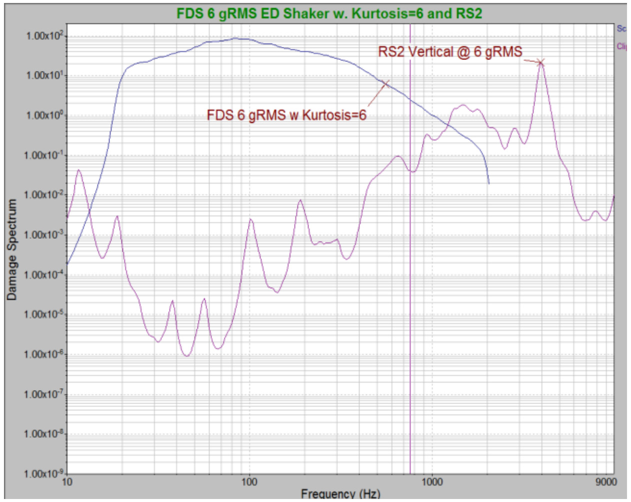
To demonstrate Analysis applications of a relative cumulative fatigue damage metric for RS machines that does not rely on the processing limitations inherent with traditional PSD and gRMS metrics:

- ***Non-Gaussian***
- ***Non-Stationary***
- ***Overlap & Averaging of FFTs -- loss of peak data***
- ***Strongly-mixed signals***

Correlations Possible with FDS



$$FDS(f) = c \sum_{n=1}^{n_f} {\sigma_n}^b$$



Crest Factor -- Kurtosis Relationship

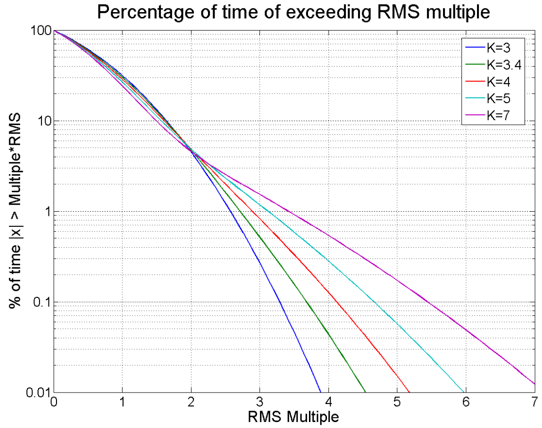
Increased kurtosis = More time at peaks

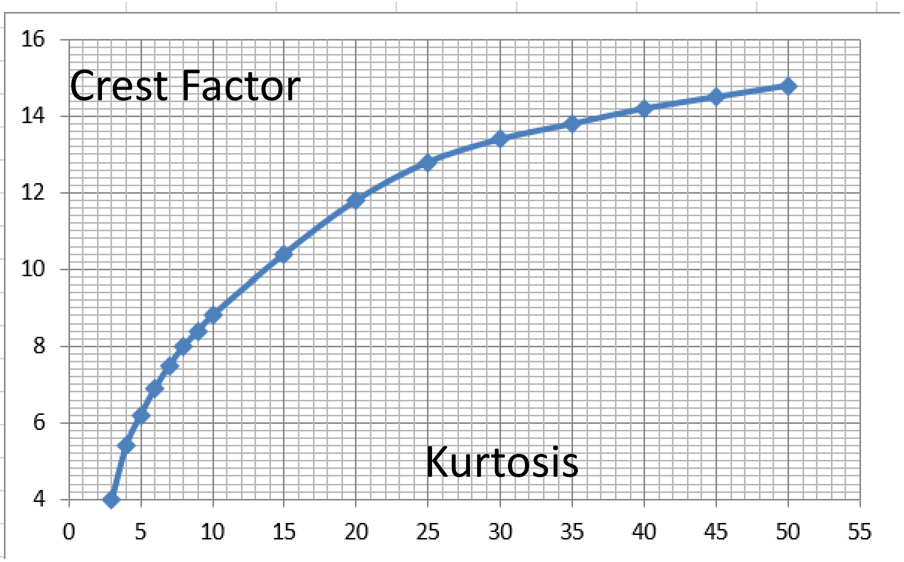
Kurtosis = 3 is > 3σ
0.27% of time

Kurtosis = 4 is > 3σ
0.83% of time

Kurtosis = 7 is > 3σ
1.5% of time

Note: 1.5% of a 1 hour test is nearly a full minute above 3σ

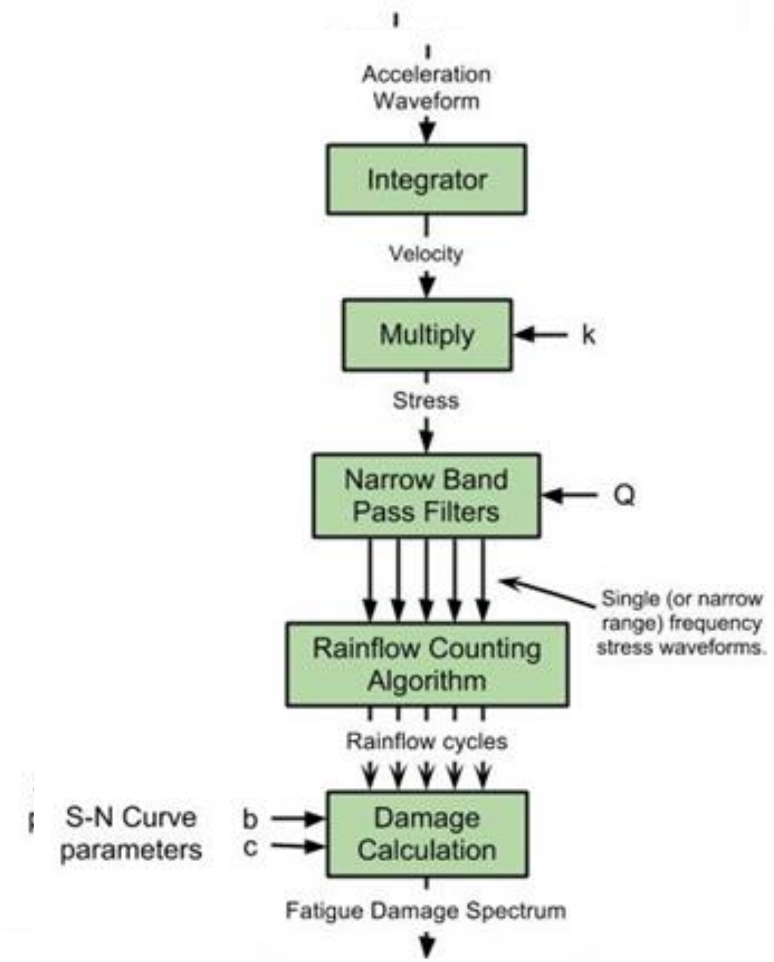




$$k = \frac{\frac{1}{N}\sum\left(x_i^4\right)}{\left(\frac{1}{N}\sum\left(x_i^2\right)\right)^2}$$

****Kurtosis is the 4th statistical moment about the mean of a data set. The Mean is the 1st, variance or standard deviation σ the 2nd, and skewness the 3rd. Kurtosis describes the "peakiness" of the data and is described by the tails of the PPD and reflects a higher incidence of higher peak amplitudes than 3 σ-limited Gaussian .**

FDS as Analysis



Don't "click" on "Create Table" which yields a Gaussian PSD and re-introduces Kurtosion to include EUE PPD peaks

Chart: Van Baren & Achatz-2014 ASTR

Benefits

FDS expands the benefits of RS machines and the HALT process by Quantifying:

- *EUEs and shaker excitations (RS and ED)*
- *Step stress levels, product strengths and margins, proof of screen, product responses and test compression*
- *Progress toward reliability and confidence goals.*
- *Analysis using FDS answers the questions–*
    - *"What are you doing to my product"*
    - *"When do I "Stop HALTING"*
    - *"How does HASS relate to HALT"*
    - *"How do I estimate reliability improvements"*

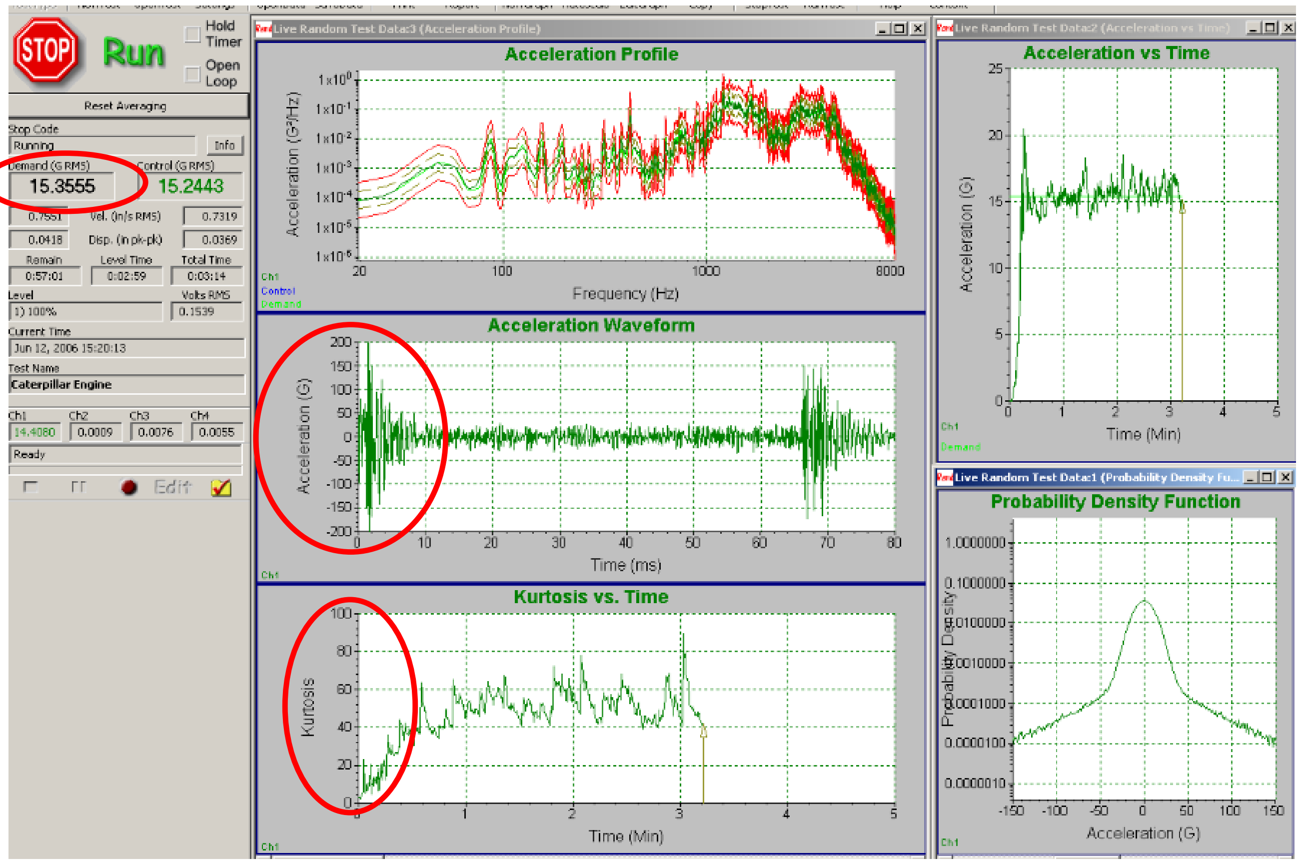
Must be a Spectrum

- ***Be it for either control or Analysis, the FDS metric must be a spectrum with selectable frequency bandwidth and resolution***
- ***Applies to all shaker types and end-use excitations and product responses—including acceleration and strain.***

$$FDS(f) = c \sum_{n=1}^{n_f} {\sigma_n}^b$$

Where *n* is the number of cycles counted by the rainflow algorithm at that frequency, and Total Damage at every frequency is the sum of the individual damages due to the cycles at that frequency, where the individual damage due to every cycle is exponential based on typical S-N curves.

Accommodate Excitations



- *Greatly different peak probability distributions (PPDs)—above gRMS=15, Peaks to 237 g & Kurtosis = 55*
- *Produce identical PSDs and gRMS which* ***Do Not*** *represent the severity of the excitation in terms of damage.*

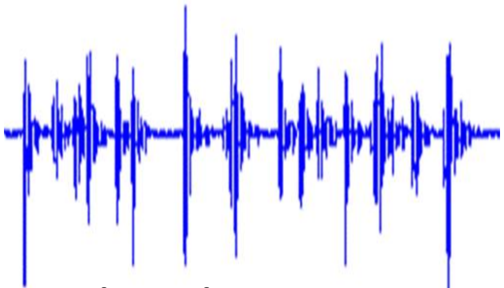
Background

- ***Dedication to a limited definition and purpose of the HALT process, "stimulate it, break it, fix it"***
- ***Acknowledging "stimulate-not simulate" and the value of feedback and corrective action***

BUT,

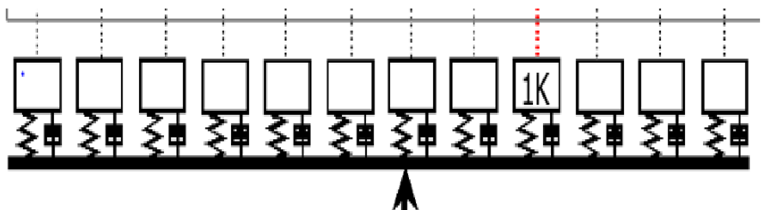
- ***No Analysis to relate the process, the test levels and the results to any other environments the product might see.***

Graphical Description of the FDS

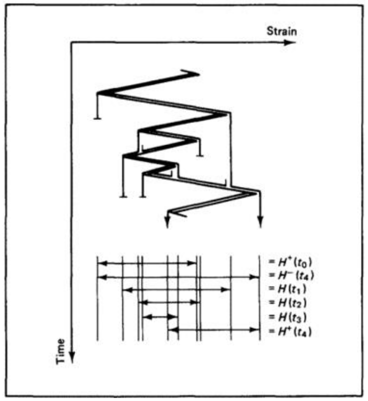


Time History

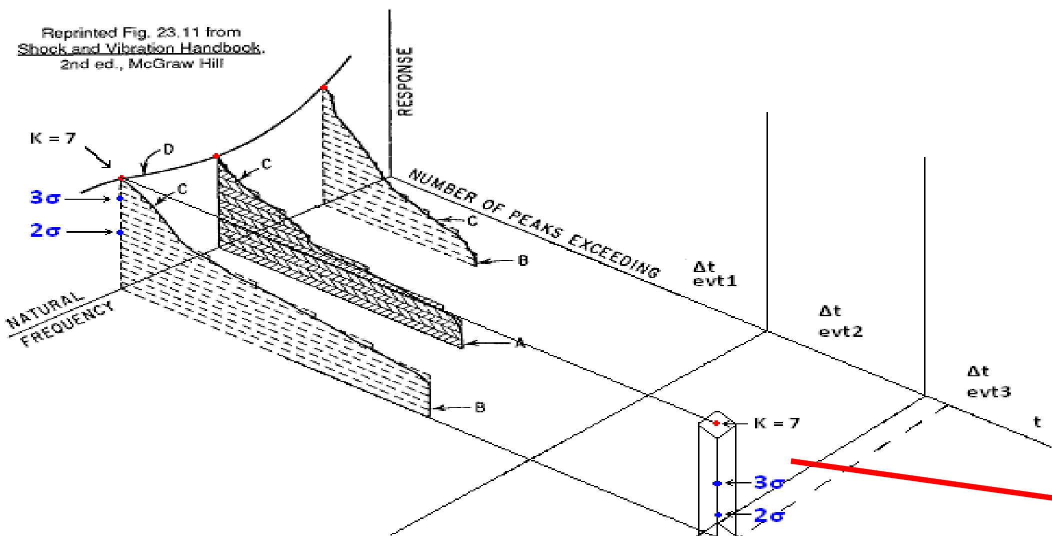
SDoF-RIRDF



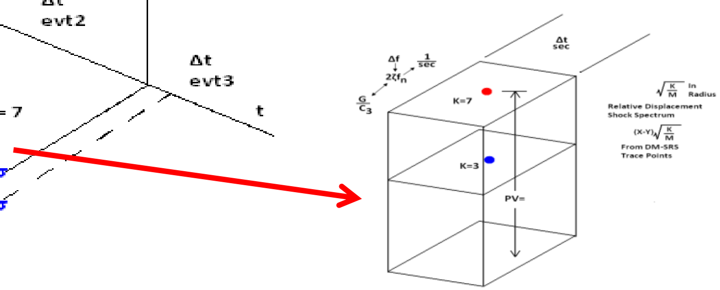
1/24th Octave Center Frequencies



Rainflow @ 1/24th Octave SD0Fs



Pseudo Velocity Response Spectrum



Insufficient Metrics- 1

- ***FFT-generated PSD is neither mathematically nor practically valid for the non-Gaussian, non-stationary excitations of repetitive shock (RS) machines.***
- ***A spectral shape and a gRMS level are not sufficient to describe an EUE, test spec, or product strength (operating and destruct limits) or service life.***

Insufficient Metrics- 2

- ***PSD is a statistical snapshot of a random process, use of PSD (g^2/Hz) and gRMS lacks elements that correlate to failure mode, fatigue cycles, field exposure with peak amplitudes more severe than Gaussian.***
- ***Does not lead to the reliability and confidence numbers (MTBF, MTBUR) or % of life used many seek from the HALT/HASS process.***

Caveats-1

- ***RS machines RS1, RS2 & RS3 are of different manufactures, vintages and designs. Their common feature is a 48" x 48" table.***

- ***Single Z axis "control" was on RS table bottoms for RS1 & RS2 and near top table center for RS3.***

- ***Unless expressly stated, reference to HALT denotes the HALT process and NOT just Repetitive Shock (RS) machines***

Caveats-2

- ***NOT a Comparison of HALT system designs or manufacturers, but FDS could be used for such.***

- ***Demonstrates a better method for doing so and quantifying relationships long ignored.***

- ***Both the PSD and the FDS lose relationships of phase and ordering of stress cycles so FDS is NOT a replication tho FDS is used to yield equivalent damage.***

- ***FDS is a means of generating a Statistically More Accurate Random Test based on cumulative damage from multiple field exposures. Summing PSDs using enveloping or a Mil-Spec formula still rely on PSD and gRMS shortcomings.***

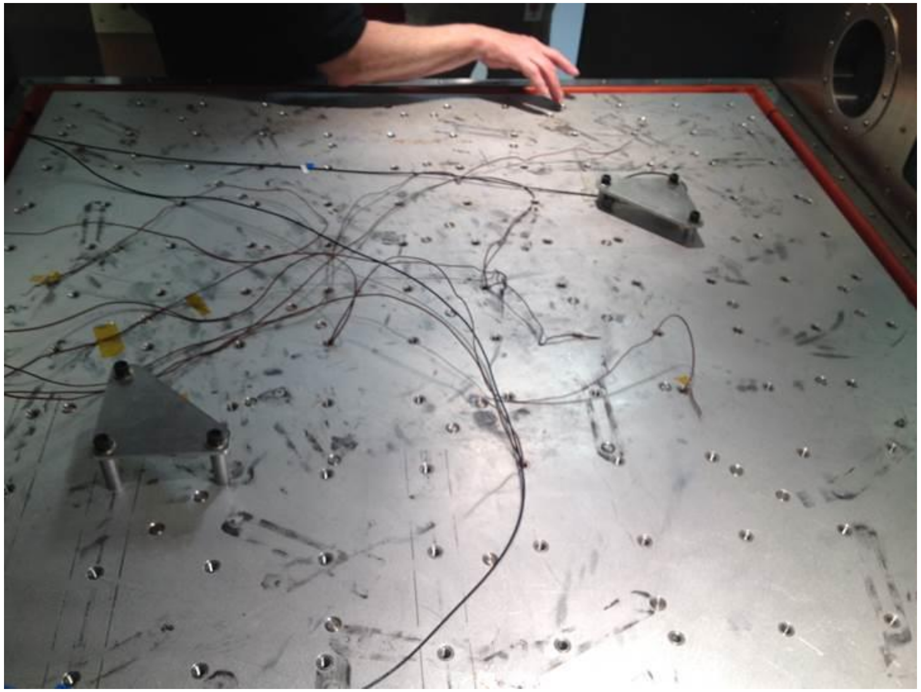
Test Set-up and Equipment

- *The early characterization of RS table performance was conducted by the late George Henderson, President of GHI Systems. George used a triangular fixture with stand-offs for the accelerometer mounting and did a* ***gRMS table spatial survey.—showing 35:1 variation in z-axis gRMS and 10:1 variations in x-y balance, again in gRMS***

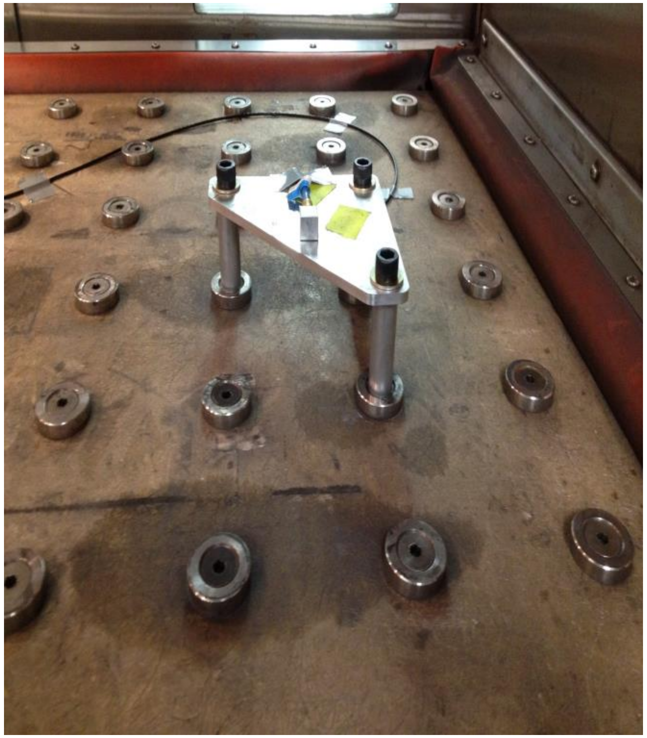
- *To allow and* ***accommodate the beneficial variations in RS machine excitation*** *due to hammer configurations, rep rates and table dynamics, this exercise utilized thinner, resonant-rich plates on 1" and 2" stand-offs, to emulate the "equally compliant" fixtures--long-recommended for pneumatic RS machines and to act as simulated product mounting points.*

- ***Data Sampled at 100 kHz for 5 minutes at each Setpoint*** *and each Fixture on each RS machine. Recorded on 2 Vibration Research VR9504s.*

RS Table & Fixtures



Triangle Fixture Locations



2” Stand-off

VR9500 Revolution – 8 Channel

Triangle fixtures F1 and F2 recorded 5 minute histories from 2 Dytran triaxes and the “control” accel from each RS machine used for closing loop gRMS setpoint with air pressure.

Time histories were streamed to the pc hard drive via VR9500s RecorderView.

Recorded Raw Data

			Z Axis Acceleration Readings on RS1, RS2 & RS3								
	Setpoint	6 gRMS		10 gRMS		20 gRMS		30 gRMS		50 gRMS	
Machine	Location	g RMS	g pk +/-	g RMS	g pk +/-	g RMS	g pk +/-	g RMS	g pk +/-	g RMS	g pk +/-
RS 1 Z Axis /	Fixture 1	14.26	443/442	32.41	262/279	37.82	422/434	103	981/727	N/A	N/A
	Fixture 2	19.38	399/350	40.05	241/230	75.2	447/452	105	784/822	N/A	N/A
	Kurtosis	K1=	8.36	K1=	4.32	K1=	6.73	K1=	3.96	K1=	N/A
		K2=	6.53	K2=	3.66	K2=	3.3	K2=	4.16	K2=	N/A
RS 2 Z Axis	Fixture 1	10.35	117/118	19.9	217/213	39.7	467/402	64.22	602/636	113	1000/923
	Fixture 2	6.35	88/86	12.48	147/145	31.7	387/321	51.56	624/521	103	1115/902
	Kurtosis	K1=	14.5	K1=	8.24	K1=	6.17	K1=	5.28	K1=	5.01
		K2=	14.2	K2=	9.19	K2=	6.02	K2=	5.91	K2=	5.63
RS 3 Z Axis	Fixture 1	15.4	89/82	24.05	137/119	41.6	418/402	55.5	410/443	52.4	1073/854
	Fixture 2	25.1	140/140	41.7	206/210	73.7	406/399	102	637/560	156	830/776
	Kurtosis	K1=	3.11	K1=	3.09	K1=	3.39	K1=	3.17	K1=	3.8
		K2=	3.29	K2=	3.03	K2=	3.03	K2=	3.04	K2=	3.06
Machine	Location	g RMS	g pk +/-	g RMS	g pk +/-	g RMS	g pk +/-	g RMS	g pk +/-	g RMS	g pk +/-
ED Shaker	Fixture 1	6.1	27/29	10	52/52	20	98/93	31	157/159	50.04	249/246
	Kurtosis*	K1	3		3		3		3		3

Table summarizes Z (vertical) axis acceleration data as excitation and responses corresponding to the RS machine "control" accelerometer.

RS2 and RS3 50 gRMS setpoints over-ranged the triax accels

Observations—Raw Data

- *The RMS levels of the RS machine excitations varied significantly from the nominal setpoint and "control" accelerometer*
- *The positive to negative g peaks far exceeded the Gaussian range expected from a random excitation. Hence the RS or Repetitive Shock designation for the machines producing a series of damped transients.*
- *For RS1 and RS2, kurtosis values exceeded the K=3 of a Gaussian peak probability distribution (PPD).*
- *As expected, Kurtosis values decrease with increasing gRMS levels.*
- *For RS3, the kurtosis values indicate a more Gaussian PPD and compare more closely with the ED shaker at the same gRMS setpoints.*
- *The variations in responses of Fixtures 1 & 2 emphasize the critical dependency on the geometry, stiffness and resonances of the unit under test (UUT) AND location on the RS table.*
- *Kurtosis values are reasonably consistent between Fixtures 1 and 2 at each gRMS setpoint level for all 3 machines.*

FDS Values

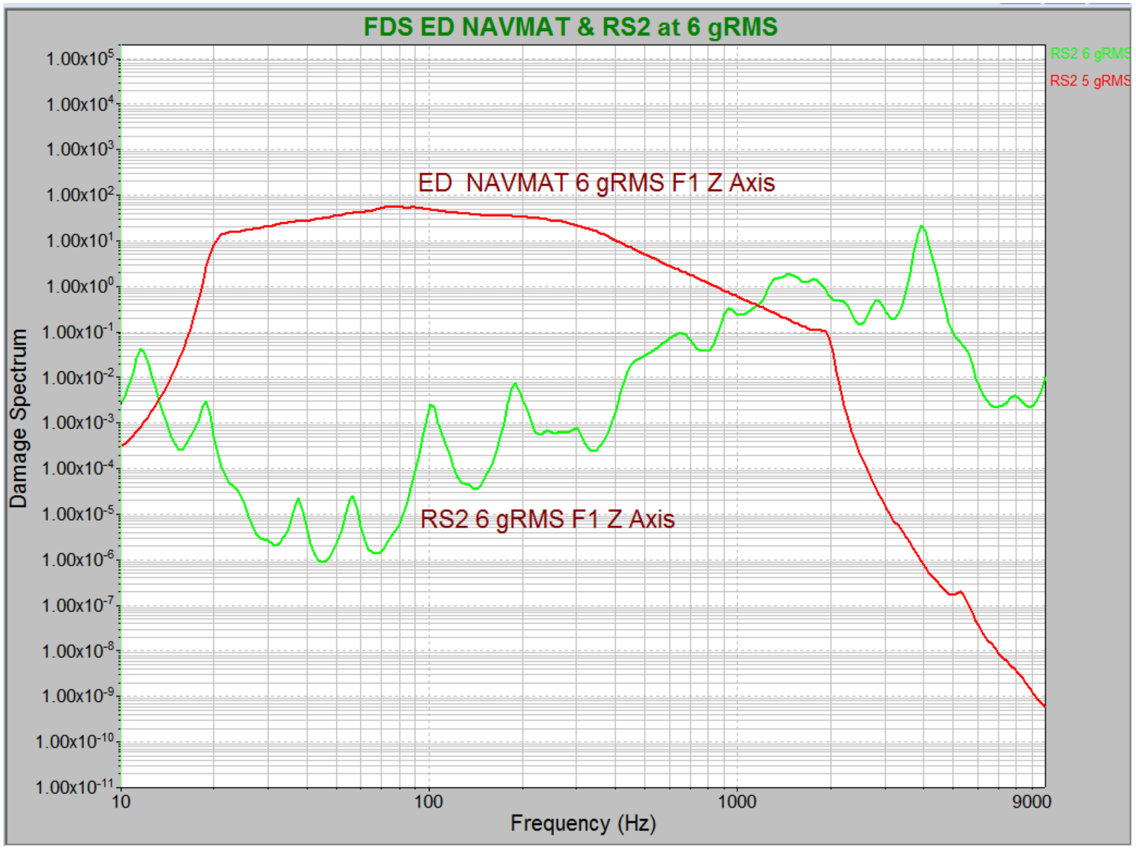
		RS2--- Input "Control" & Responses				
		Fixture 1 with 1" Stand-offs				
Setpoint						Combined
		CONTROL	X1-Ch2	Y1 Ch3	Z1 Ch 4	X1+Y1+Z1
6 gRMS		110	125	64	74	263
10 gRMS		570	433	414	1175	2019
20 gRMS		6596	11321	8829	30559	50709
30 gRMS		36938	102661	62059	225923	390643
50 gRMS		116808	236245	236245	1700371	2172861
		Fixture 2 with 2" Stand-offs				
		CONTROL	X2 Ch 5	Y2 Ch 6	Z2 Ch 7	X2+Y2+Z2
6 gRMS		110	124	516	601	1242
10 gRMS		570	841	516	601	1959
20 gRMS		6596	30559	18180	10386	59126
30 gRMS		36938	147632	89835	252272	489740
50 gRMS		116808	587214	337916	2380313	3305443

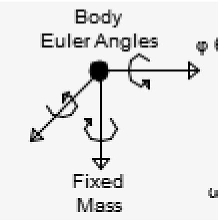
Cells represent the FDS sums for 2 fixtures:

- 5 minutes @ each Setpoint
- X, Y & Z + Combined
- Non-linear w. set-points due to hammer rep rates, table and fixture geometry & structure and # cycles of rep rate harmonics

ED Shaker and RS Machine-Basic Comparison

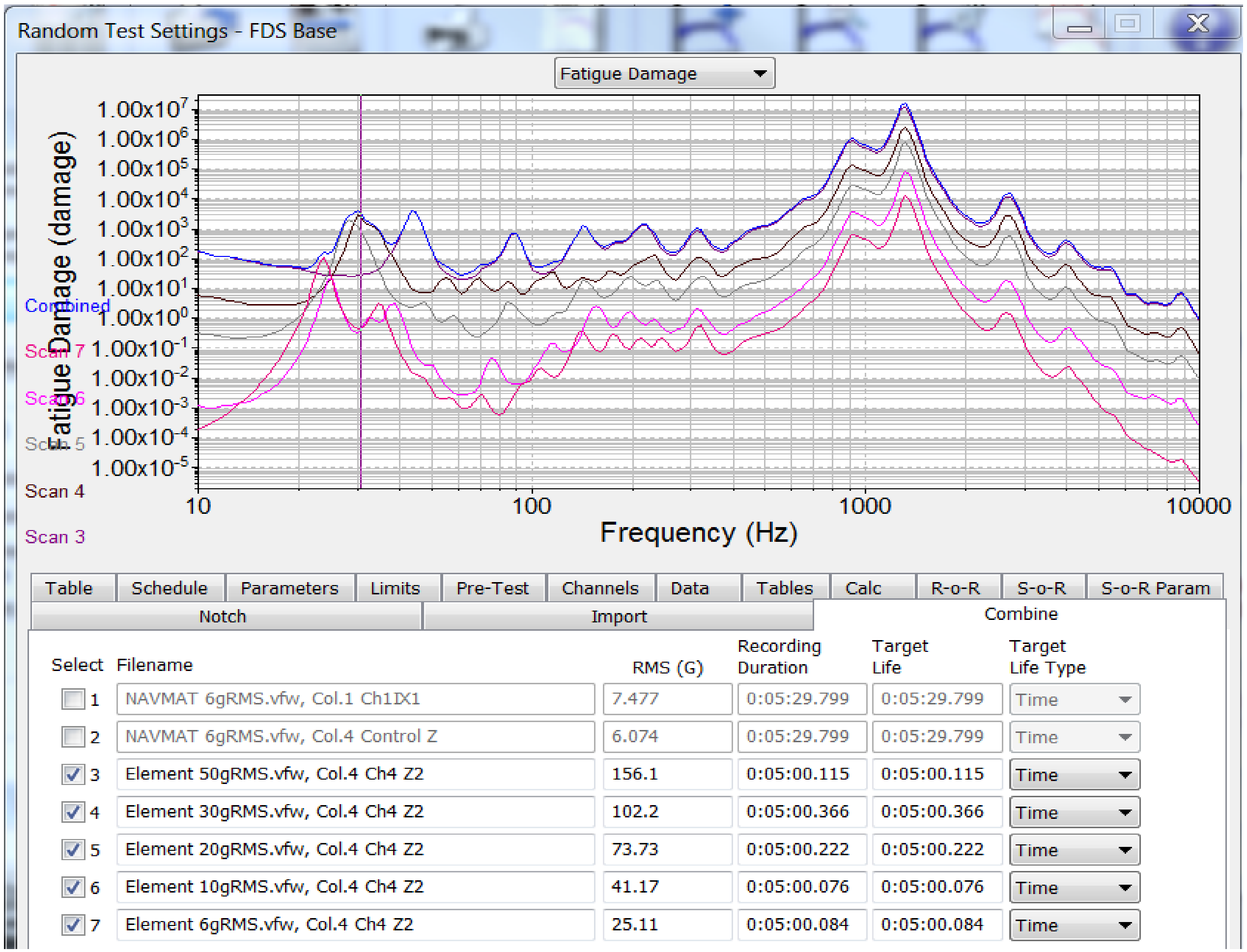
- *ED NAVMAT 6 gRMS- all frequencies simultaneously*
- *Damage Cross-over is approx 1100 Hz.*
- *Different bandwidths excited by ED & RS machines.*
- *Compare With UUT frequency response plots.*





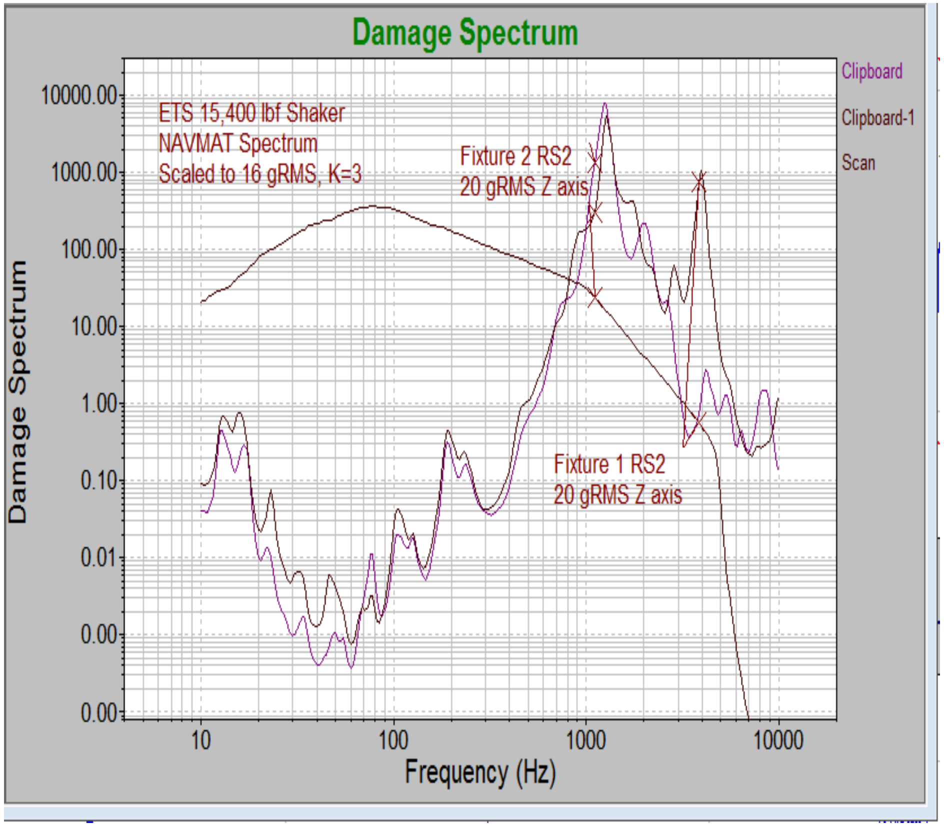
Bandwidths of Less Damage Capacity

Step Stress 6, 10, 20, 30 & 50 gRMS + Combined



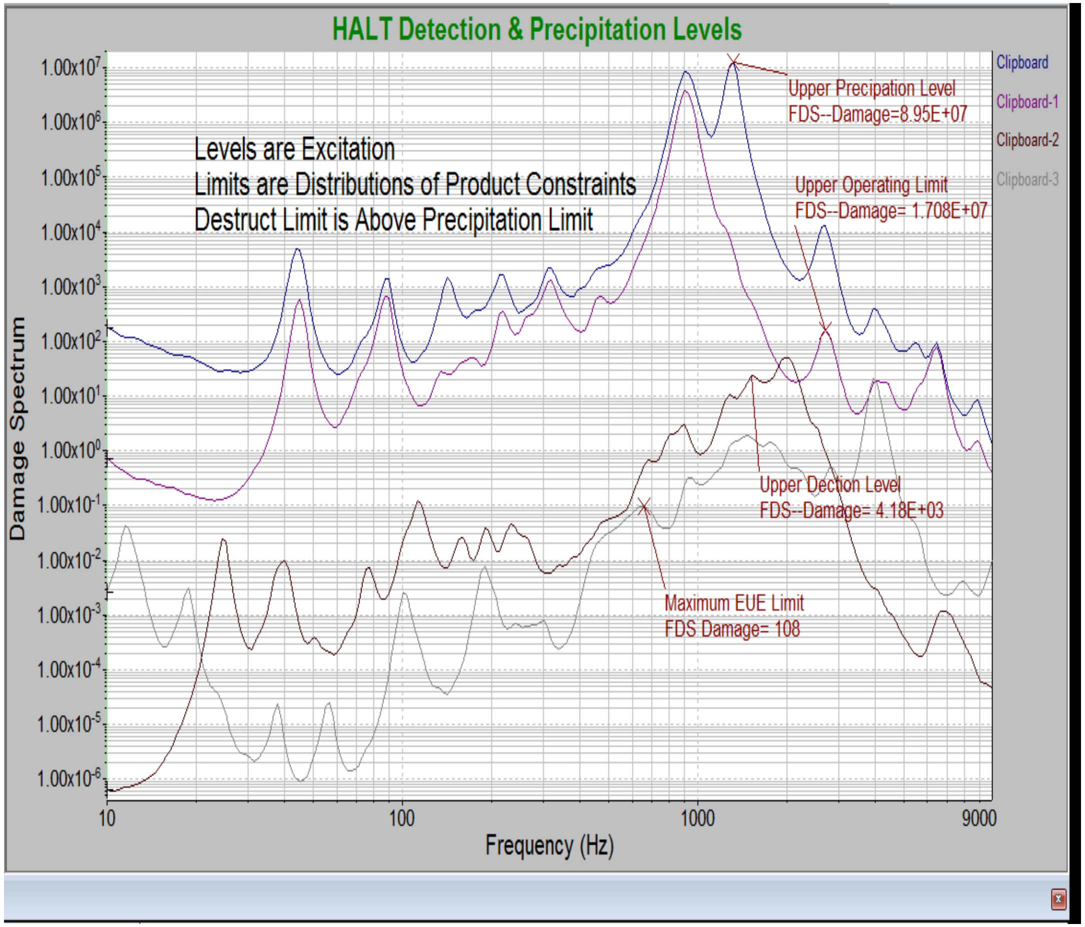
- **Documents a HALT step stress progression in terms of damage. Also product responses.**
- **Combined trace is the "global" sum of the damage from 6, 10, 20, 30 and 50 gRMS setpoints for RS machine 2, analogous to the gRMS power of a random test.**
- **With powered and monitored product and outputs, product failure or parameters exceeding acceptance limits can send an alert of "Limits Exceeded" or abort the test**
- **Cumulative damage to time of failure or limit exceedance.**

RS2 at 20 gRMS vs. NAVMAT to 4000 Hz at 16 gRMS



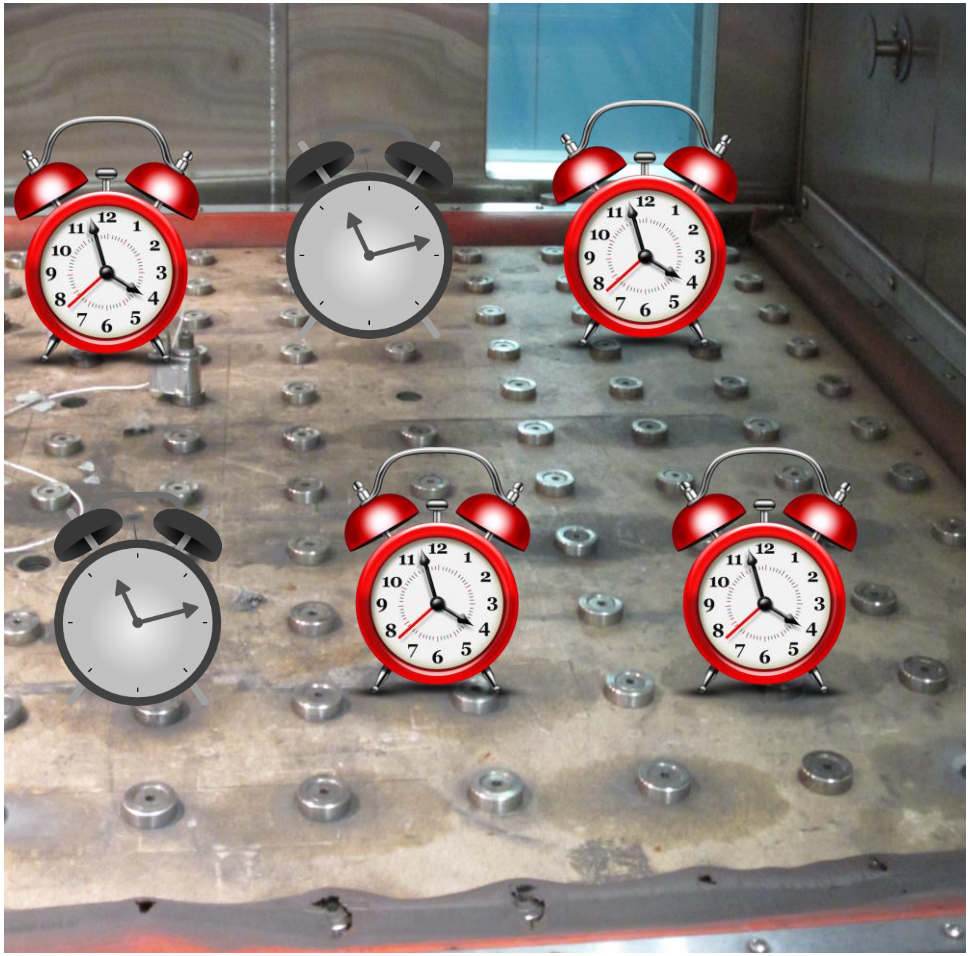
- FDS of NAVMAT "haystack" spectrum on an ED Shaker @ 6 gRMS and K=6 to 4 kHz compared with RS2 @ 6 gRMS setpoint.
- The frequency bandwidths to excite UUT Resonances differ significantly. Damage cross-over is approximately 1300 Hz
- Allows trade-off of Gaussian random with Kurtosion with increased gRMS power to achieve peak accelerations of the EUE.

Precipitation & Detection Levels



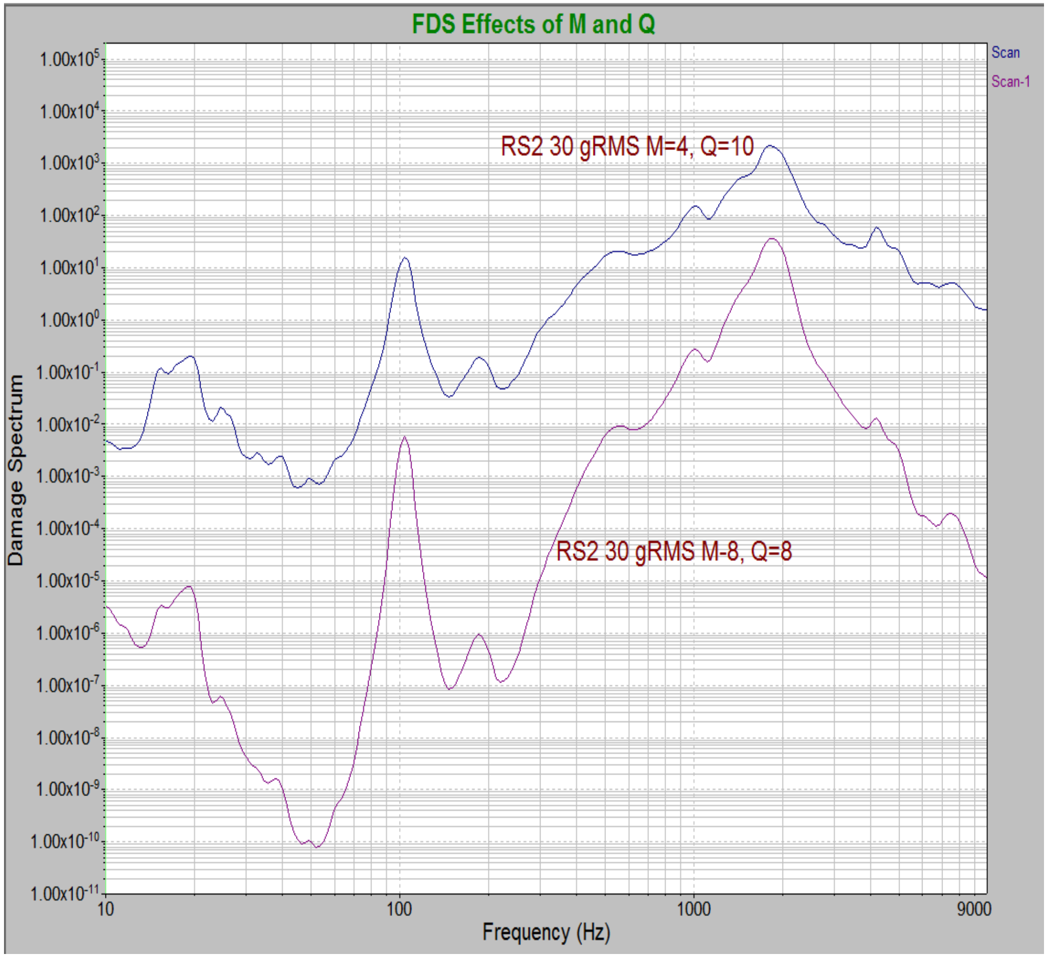
- **Step Stress Levels can be related to the Detection and Precipitation screen in terms of damage via the FDS.**
- **Proof of screen and UUT exposure to HASS levels can be generated as a % of the FDS cumulative HALT damage achieved.**
- **Or, as a % of cumulative life model derived from multiple time histories and weighted proportions via FDS.**
- **Recall that each level is a distribution, not an discrete value.**

Managing Multi-UUT HASS



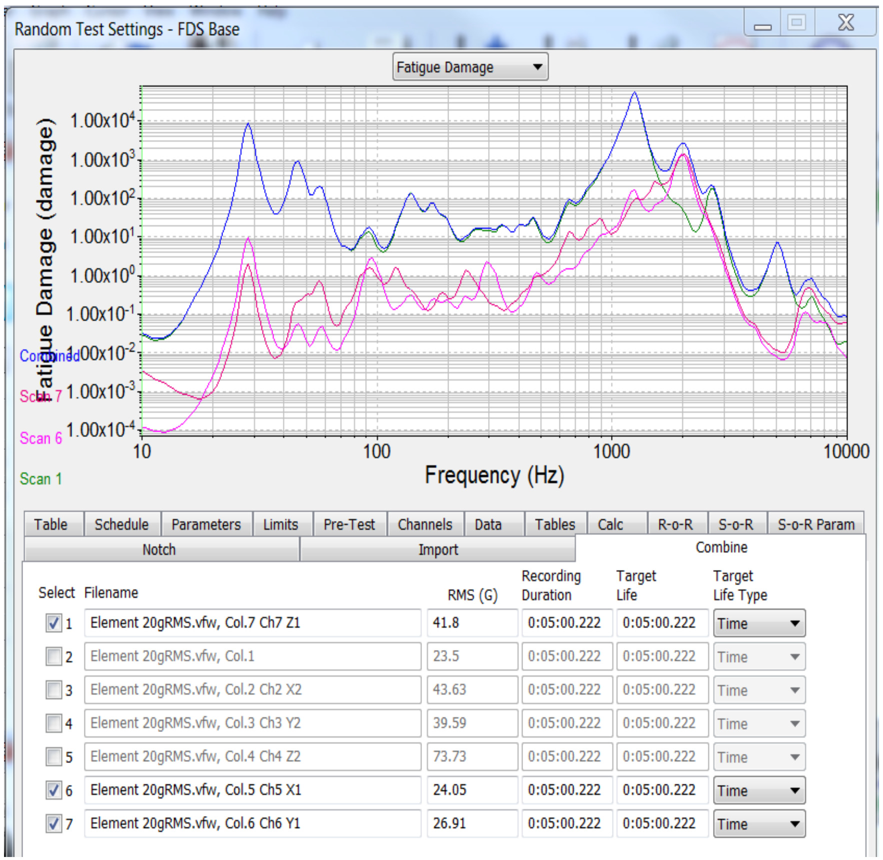
- *HASS FDS scaled from HALT FDS Damage Sum*
- *Monitor at product/fixture or response locations*
- *Accommodate w. fixtures*
- *Remove and replace w/r time to achieve equal exposure*
- *The "Fatigue Clock"*

FDS for Assembly Input & Response



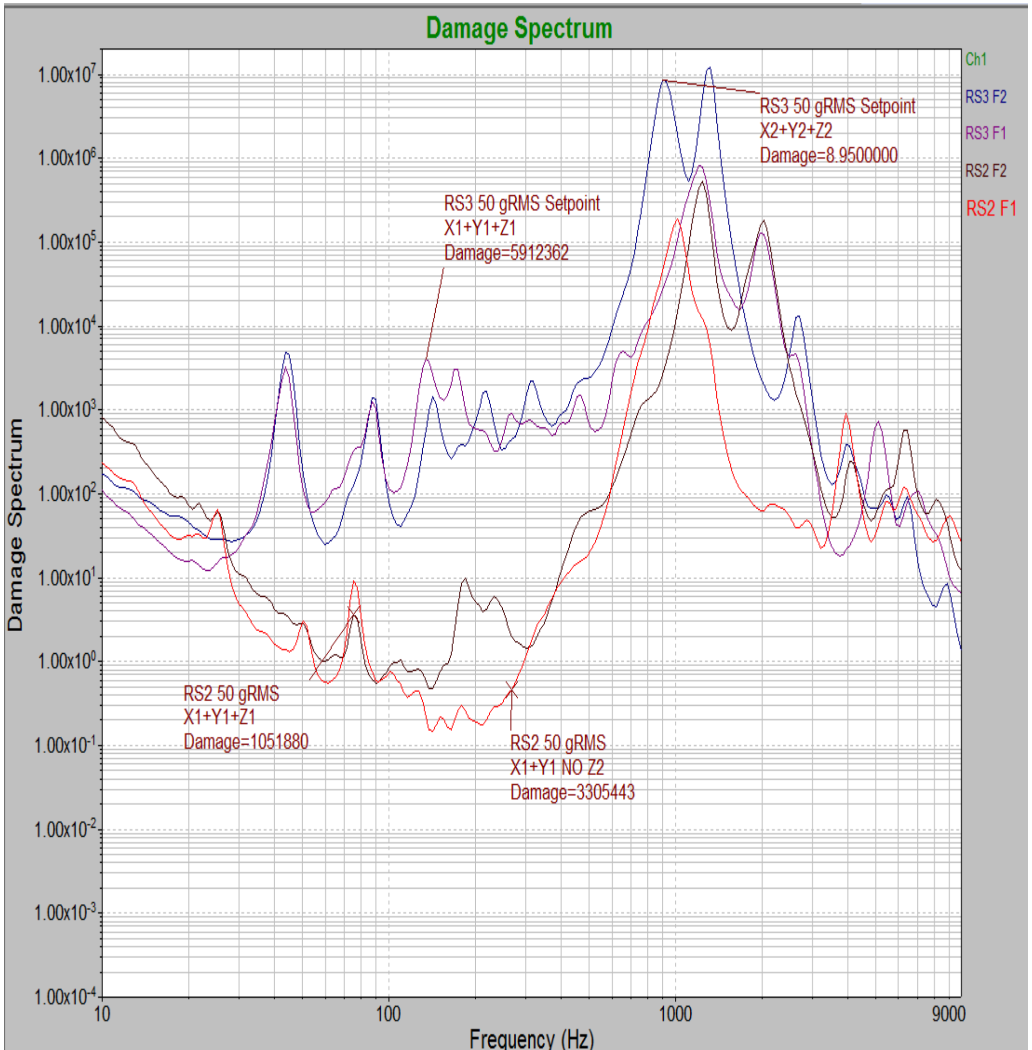
- Select “m” & “Q” specific to assembly material & resonances @ UUT Location
- E.g., Compare response w. input across Fuel Tank Mounting Brackets
- Shown: same time history, vary “m” and Q”
- An FDS Transmissibility—use bandwidth cursors

Global 3 Axis Damage Sum



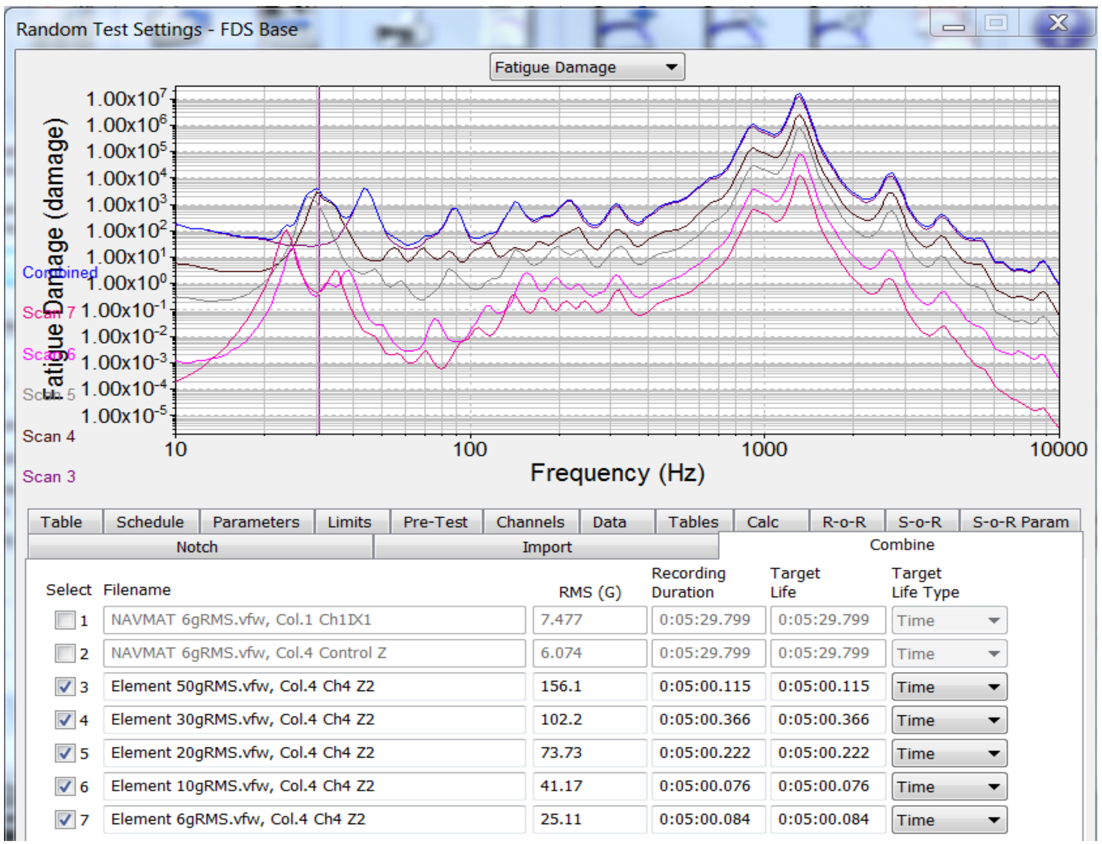
- **Combining the FDS damage traces from orthogonal axes (X1+Y1+Z1) provides a global indication of the 3 DoF severity of RS machines.**
- **The summation includes cross-coupling between axes, but still presents a spectrum.**
- **Can’t do with PSDs and gRMS**
- **The UUT structural stiffness, resonant responses and damping remain variables in the path to a more precise solution**
- **The UUT response functions can be compared with the excitations to identify resonant response half-power bandwidths of potential damage.**

Combined
X, Y & Z FDS w. Damage Sums



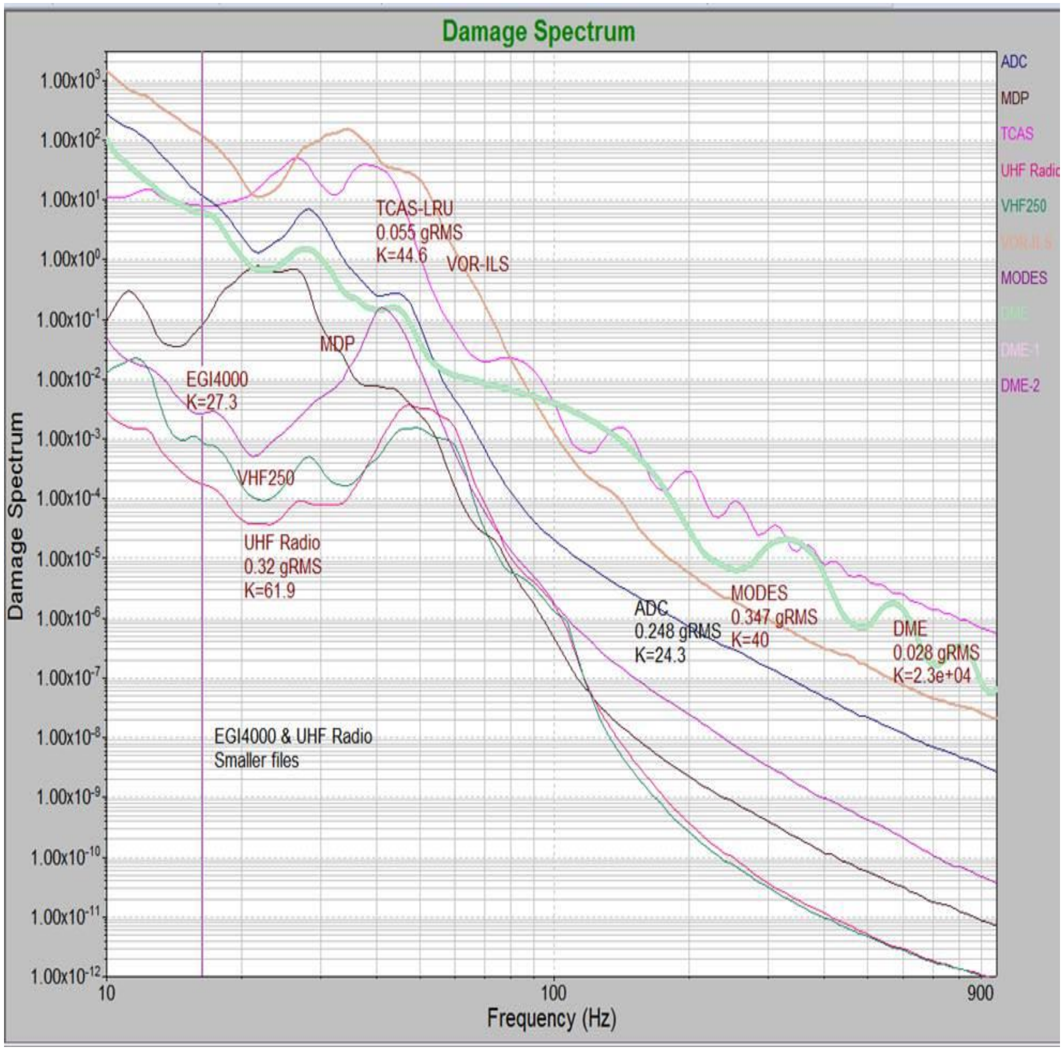
- **FDS for RS2 & RS3 @ 50 gRMS setpoint with Damage Sum.**
- **Both F1 and F2 fixtures shown for RS2 & RS3 Machines**
- **Damage Sum is the sum of all 1/24th octave points on the FDS -- broadband or selected bandwidths.**
- **The “volume integral” described above and is a global indicator of the total damage**
- **Tool for comparison with other RS machines, ED shakers, EUEs and test specifications.**
- **Or, envelop multiple FDS to get “maxi-**

Comparison of HALT Margins with Product Service Life Profile



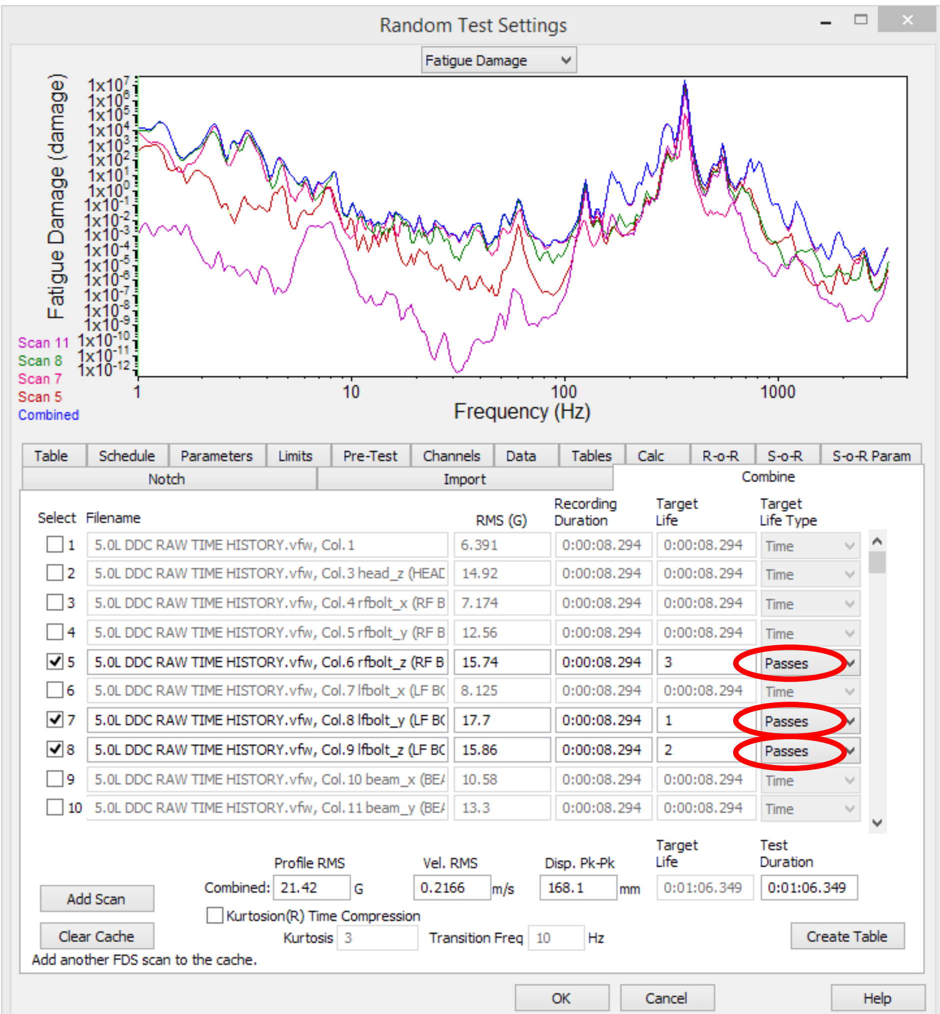
- **Example:**
  - **Middle FDS traces represent the FDS damage from 6, 10, 20, 30 and 50 gRMS HALT levels**
  - **Top FDS trace represents total Combined HALT level achieved representing fundamental limits of design**
  - **Lower trace represents the product service life in terms of damage of the weighted multiple imported product EUE time histories. .**
  - **Conclude the product has been HALTed 10 x projected life**

EUE Comparison



- *T-38 Cockpit*
- *9 Avionics boxes*
- *1 hour flight each*
- *Failures in service @ 20% of production build*

Define/Spec Service Life



Suggested Field Exposure for Customer Profile

Fuel Rail EUE

Product vibration specs be augmented in terms of FDS– cumulative damage incorporating EUE kurtosis and cycle-counting.

A Gaussian spectrum can be generated from FDS and Kurtosion© re-introduced.

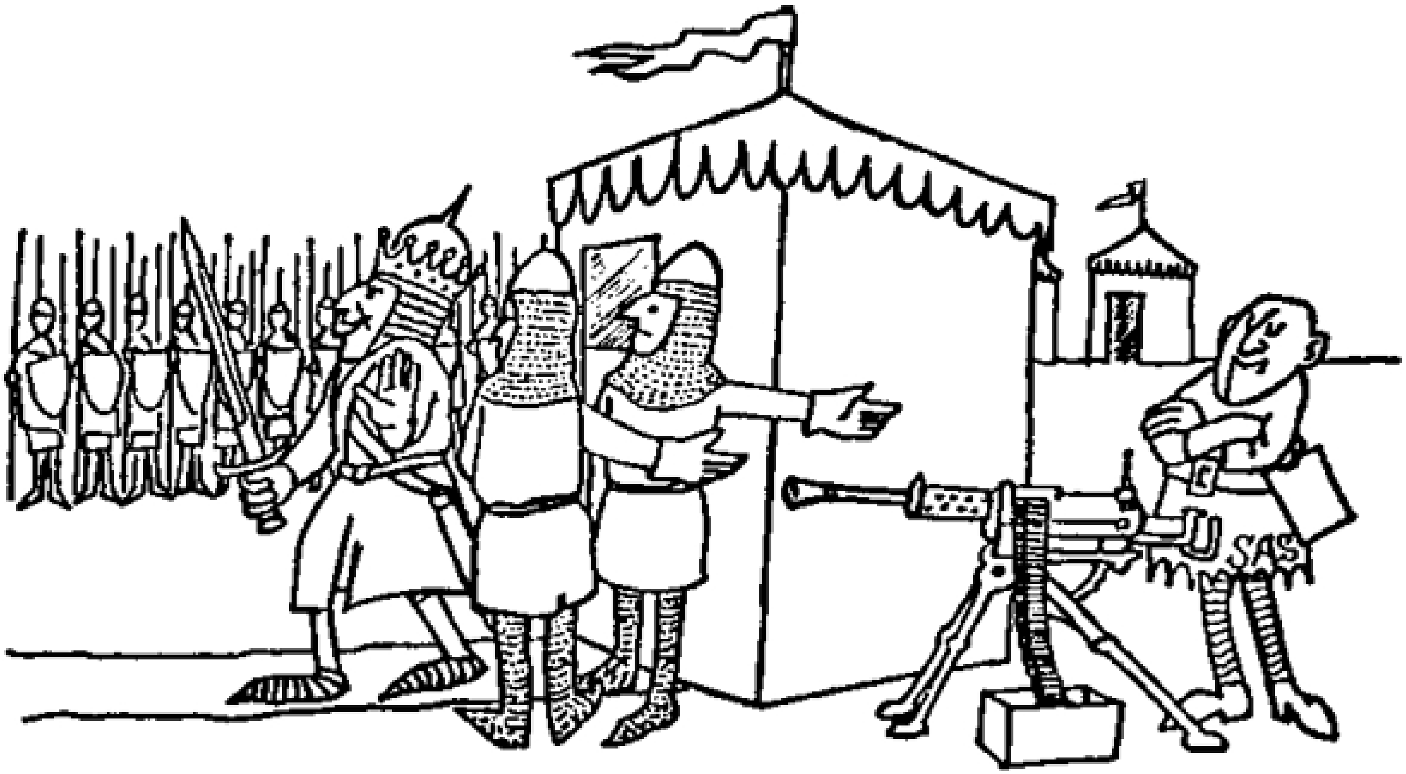
The approach improves test tailoring, eliminates the shortcomings of PSD and attendant gRMS metrics and is applicable to EUE and all shaker excitations.

Based on velocity of first bending mode, FDS is proportional to stress and accommodates multiple EUEs and weighting for duty cycle. It applies to strain as well.

Recommendations

- *Relate product strengths achieved in HALT to derive margins above EUE, qual test specs, reliability growth and FDS models of service life.*
- *Use FDS with higher channel counts for comprehensive table mapping, fixture analysis and UUT response.*
- *RS machine table variations can be managed using FDS as the "Fatigue Clock" to track multiple UUTs undergoing HASS with FDS updates. Relate HASS to HALT.*
- *The FDS tool can be of value quantifying single axis and simultaneous 3 axis ED shakers proposed for HALT processes and on product not sufficiently stimulated by RS machines.*
- *FDS can be used to evaluate cross-axis inputs from ED shaker with different suspensions.*
- *Should designer engineers and Physics of Failure (PoF) investigators pursue relative contributions of RS machine cross-axis and rotational inputs, product and component assembly responses can be better evaluated.*

Thank You



"No! - I can't be bothered to see any crazy salesman - we've got a battle to fight!"